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N8120R:72-030

ENGINEERING OPERATIONS REPORT

NERVA DYNAMIC ANALYSIS METHODOLOGY

-SPRVIB-

PROJECT 187

(NASA-CR-132214) N73-24671 NERVA DYNAMIC ANALYSIS METHODOLOGY, SPRVIB (Aerojet Nuclear Systems Co., Azusa, Calif.) 75 p HC \$5.75 CSCL 21F Unclas

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D. F. VRONAY

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APPROVED:

U. A. PINEDA, MANAGER

APPLIED MECHANICS

ENGINEERING STAFF DEPARTMENT

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CLASSIFICATION CATEGORY

NERVA DYNAMIC ANALYSIS METHODOLOGY

-SPRVIB-

I. INTRODUCTION

This report documents the general dynamic computer code called SPRVIB (Spring Vib) developed at Westinghouse Astronuclear Laboratory in support of the NERVA (Nuclear Engine for Rocket Vehicle Application) Program. Using normal mode techniques, the program computes kinematical responses of a structure caused by various combinations of harmonic and elliptic forcing functions or base excitations. Provision is made for a graphical type of force or base excitation input to the structure.

II. SUMMARY AND CONCLUSIONS

The usefulness of a dynamic computer code can be determined by examining four main features:

- 1) the method of solution
- 2) the type and generality of the forcing functions used
- 3) the flexibility of the input/output routines
- 4) size limitations of the program caused by storage and/or computational limits

The computer code, SPRVIB, should then be examined for all of these features.

A description of the required input format and a listing of the program are presented, along with several examples illustrating the use of the program, in Reference 1. SPRVIB is written in Fortran IV computer language for use on the CDC 6600 or the IBM 360/75 computers.

SPRVIB was used by ANSC for the dynamic analysis of the NERVA 400D and 400D' engine configurations. For the 400E configuration it was not used at all due to the loss of in-house computing facilities, the limited size of the program, and the adoption of the NASTRAN program as the standard analysis tool for the structural dynamics group.

III. TECHNICAL DISCUSSION

SPRVIB uses a classical normal mode solution in which the individual response is computed as a sum of all the modal responses. This type of solution has two main advantages:

- 1) It completely describes the structure and often enables one to estimate the frequency dependence of the structure. This, of course, is not possible with a numerical solution.
- 2) It enables the exact solution to a linear problem to be determined in closed form if the forcing functions can be described by elementary functions. In these cases, roundoff type errors do not accumulate.

A normal mode solution also has two disadvantages:

- 1) At each time step in a transient solution to be printed out, conversion must be made from the normal coordinates to the physical coordinates of the problem.
- 2) Only proportional damping or modal damping type solutions are tractable for general programming.

The first disadvantage does not appear to be limiting in these days of the high speed computer. If the forcing functions are easily describable, such as harmonic or elliptic functions, the solution obtained is exact at each time step and the step size can be determined by convenience or plotting limitations. On the other hand, the time step size of the ordinary numerical type solutions determines the accuracy and stability limitations of the solution. Furthermore, with the possible exception of physical damping instruments, the damping constants used in dynamic analysis are usually crude estimates of the actual damping. As such, it would appear at least as correct to use estimates of modal damping constants which often may be obtained from test results. Hence, the apparent limitations are often not applicable to practical problems.

SPRVIB offers the following wide variety of possible forcing functions:

1) Free vibrations with arbitrary initial displacement and velocities at each generalized mass.

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2) Arbitrary harmonic forces $F_0 \sin \omega t$ acting at each or all of the generalized mass points. Forces with different amplitudes and frequencies can be simultaneously applied at the various points.

- 3) Elliptic type forcing $F_0 \exp(\beta t)$ can act at each or all of the points similar to that described above. The parameters F_0 and β are real parameters which may have different values in as many as four consecutive time regions. Using this type of representation, a shock or explosive type of forcing can be easily described with sufficient accuracy to obtain quite accurate estimates of even velocities and accelerations. In addition, the harmonic and elliptic loads may be superimposed at any point.
 - 4) Base harmonic excitation of the supports.
- 5) Point force input at any mass point. In this case the force is represented as a set of data points.
- 6,7,8) Base motion in which the support acceleration (velocity, displacement) is described by a set of data points.

The effectiveness of the input and output features of any program greatly affect the time a user must spend in setting up a problem and the practicality of its use. A limiting feature of most dynamic computer codes available at this time is the requirement that the element matrices, such as the stiffness matrix, be generated by the direct stiffness method or some other similar method. SPRVIB will generate the element matrices for discrete mass elements connected by rigid bars, linear and rotational springs, and viscous damping elements. Besides the regular input options, provision is made to input only the non-zero symmetric elements of sparse matrices. This provision was used exclusively for the NERVA dynamic analysis. This option is very useful for large matrices. All the input can be in a punched card format or some matrices can be read in from magnetic tape.

An option is available to store all the matrices and results from the topological portion of the program, including the mode shapes and frequencies, on tape so that this section of the program will not have to be redone at a later date for further load cases on the same problem. Any transient information which

can be printed out can also be stored on tape for possible future plotting. Besides the regular steady state response, provision is made to output the results of each harmonic or elliptic load acting separately as well as the combined effect for each load case. In this way the transient effect of each load may be determined with a coarse time step while the effects of the combined loadings can be determined with a finer time step. One, two, or all of each of the displacements, velocities and accelerations may be output at each time step.

At the present time SPRVIB is limited to 90 degrees of freedom. The storage requirement of the program with the 90 degrees of freedom is $175,000_8$.

The detailed program write-up, including a listing of the program, is contained in Reference 1. The remainder of this report illustrates a typical application of the program to the 4000' engine analysis.

Figure 1 shows the dynamic model of the 400D' engine, consisting of massless beams connecting a series of concentrated masses so distributed as to approximate the mass distribution of the engine. Table 1 is a list of the degrees of freedom and what physical interface they represent.

The input to SPRVIB consisted of the diagonal mass and damping matrix, the stiffness matrix and a specification of the input/output control parameters.

The output consisted of an echo of the mass, damping and stiffness matrices, a list of the non-zero entries by vector locations, and a row by row printout of the final stiffness matrix. This is followed by the calculated output consisting of the damping constants, and finally the eigenvectors and corresponding natural frequencies. These modes are then used, together with the transformed input, to perform, in this example, the transient response analysis due to a base input acceleration of 0.3g. Two types of output are presented. First, a summary of the peak response at each degree of freedom. This is then followed by the actual time history of the coordinate displacements, velocities, and accelerations.

The output from this sample run appears as Appendix A. Only a portion of the time history response is shown.

IV. REFERENCES

1. "SPRVIB A General Purpose Dynamic Computer Code Using Normal Mode Solution", Westinghouse Astronuclear Laboratory Report WANL-TME-1940, June 1971

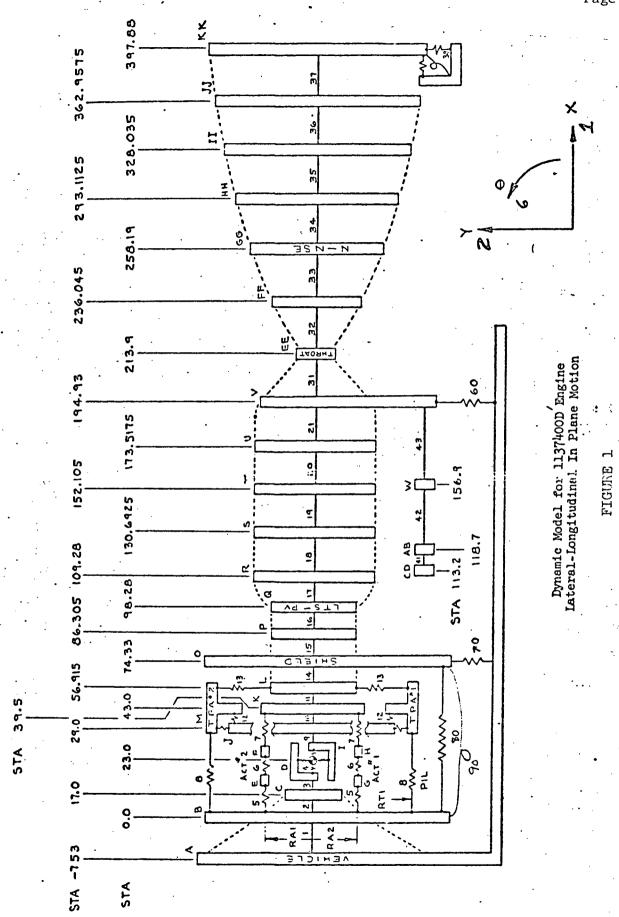


TABLE 1
DEGREES OF FREEDOM

Point	<u>X</u>	<u>Y</u>	<u>θ</u>	
A	1	2	3	Stage
В	4	5	6	Interface (Stage/Upper Thrust Structure)
C	7	8	9	Upper Thrust Structure/Gimbal
D.	10	11	12	Gimbal Pivot Forward
Ε.	13	_	-	Actuator #1 Forward End
F	14	-	·	Actuator #1 Aft End
G	15	- ,	-	Actuator #2 Forward End
H	.16	-	_	Actuator #2 Aft End
I	17	18	19	Gimbal Pivot Aft
J	20	21	22	Gimbal/Lower Thrust Structure
K	. 23	24	25	Lower Thrust Structure-
L	26	27	28	Lower Thrust Structure
. M	29	30	31	TPA #1
N	32	33	34	TPA #2
0	35	36	37	Shield
P	38	39	40	Lower Thrust Structure
Q	41	42	43	Lower Thrust Structure/Pressure Vessel
R	44	45	46	Pressure Vessel
S .	4.7	48	49	Pressure Vessel
T	50	51	52	Pressure Vessel
U .	53	54	55	Pressure Vessel
V	56	57	58 ~	Pressure Vessel/Nozzle/Nuclear Subsystem
CD	5 9	60	61	Nuclear Subsystem
AB	62	63	64	Nuclear Subsystem
W	65	66	67	Nuclear Subsystem
AY	-	68	-	Stage
EE	69	70	71	Nozzle Throat
FF	72	73	74	Nozzle Divergent
GG	75	76	77	Nozzle Torus/Extension
HH	78	79	80	Nozzle Extension
11	81	82	83	Nozzle Extension
JJ	84	85	86	Nozzle Extension

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DEGREES OF FREEDOM (Cont.)

Point	X	<u>Y</u>	<u>θ</u>	
KK	87	88	89	Nozzle Extension/Destruct Subsystem
*LL	90	91	92	Destruct Subsystem

^{*}The Destruct Subsystem parameters are set to zero to eliminate it.

APPENDIX A

TYPICAL RUN

SAMPLE OUTPUT

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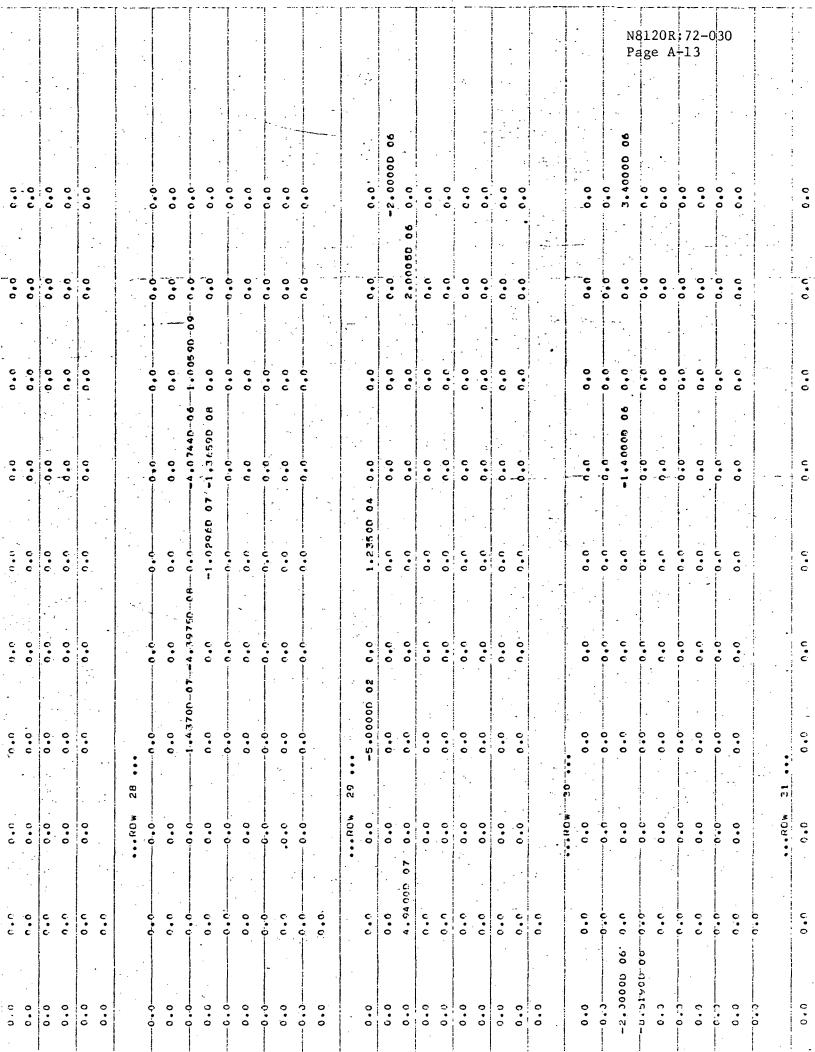
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-2.34360 66	4.70700 08		0.0	0.0	0.0	0.0		0.0	0.0	30
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0•0	0.0	· · · · ·	0.0	0.0	0.0	0.0	0.0	
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C • 0	υ•υ	0.0	0.0	0.0	0.0	0• 0	0 • ن	. U*U	0.0	

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6.0	0.0	0.0	0.0	0.0	0.0	0.0	-7.8130D 07	-2.34380 08	0.0	
e.7630D C7	-2.01650 08	0.0	-5.50000 06	2.50000 07	0.0	0.0	0.0	0.0	-2.0000D 06	
2.3000D C7	0.0	-2.000UC 06	2.8000D 07	0.0	0.0	0.0	0.0	0.0	0.0	
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0.0	0.0	0.0	٥•٥	0.0	0.0	0.0	0.0	0.0	0 • 0	
(•)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0•0	, 0•0	
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. 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0•0	
٠٠٥	C • C									
		ROW 22							es de companyation de la companya de c	
0.0	0.0		0.0	0.0	0 • 0	0.0	0.0	0.0	0.0	
i		0.0	0.0			0.0	-2:3440D-CR	4.7070E 08	0.0	
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٥•٥	0.0	0.0	0.0	0.0	. U•0	0.0	. 0•0	0.0	0.0	
C0	v •0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	***************************************
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		ROw 23	•				**			
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2.30005 C7	9.25000 07	-5.62500 07	•	2.26620 09	0.0	-1.43650 07	-4.39750 08	0.0		
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0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
C • O	٥•٥	. 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
C•0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
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		ROW 38	•								
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C • 0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	
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0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0		
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	•	. ROW42						٠. ٠			
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o•o	20 000000	1.2697C 08		-7.52700 07	1.35000 08	0.0	0.0	0.0	0.0		
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· · ·	. -				•					*****
		WOW 47	•							
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0.0	0.0	0.0	0.0	, U•0	0.0	0.0	0.0	0.0	0.0	
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0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	****
0.0	0.0	0.0	-5.89800 07	0.0 7	0.0	1.17960 08	0.0	0.0	-5.2980D 07	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
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0.0	ى• o	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0			• •		•				
		RUW 48								
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
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0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0-	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	1.0870D-07	71-1-6350-08	0.0	2-1-74-00-07	-4.6125D-04-	0.0	
-1.08700 C7	1.16400 08	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0 • 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0 (c	0 0	0.0	0 0	0 4	0.0	0.0	0.0	0.0	
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		ROW 49	•				•			
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0.0	0.0	. 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	†
0.0	0.0	0.0	0.0	0.0	0.0	0.0	. 0.0	0.0	0.0	
0.0	0.0	0.0	0.0	1.16400 08	8 -2.05080 10	0.0	-4.61250 04	4.5999D 10	0.0	N8 Pa
-1.16350 CB -	-2.050BD 10	0.0	0.0	0.0	C. 0	0.0	0.0	0.0	•	120 ge
0.0	0.0	0.0	0.0	0•0	0.0	0.0	0.0	0.0	ر د• ٥	OR A-
(.•0	0.0	0*0	0.0	0.0	Ú•0	0.0	0.0	0.0		72
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	e en esta esta de amendo debasea de debasea, en en el debe sente		annumber of marks and marks before a construction.						The state of the s	
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ů.1	0.0	0.0	0.0	0.0	0.0	0	0 0	0 0		

	•	5° 4	r. • c	0.0	u*0	u•0	0•0	0.0	0.0	
	0.0	0.0 -5.8980F 07	0 0	c (-5.8980D 07	0.0	0.0	1.17960 08	
0.0	· · · · · · · · · · · · · · · · · · ·	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-	0.0	
0.0	0 · 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0•0	
				-						
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0.0	Ú•0 ·	0.0	0.0	0.0	0.0	0.0	0.0		0.0	
0.0	0.0	0.0	0.0	0.0	0•0	0.0	0.0	0•0	0•0	
0.0	0.0	İ	0.0	0.0	0.0	0.0	-1.08700 07	-1.16350 08	0.0	•
2.17400 07	-4.61250 04	0.0	-1.08705 07	1.16405 08	0.0	0.0	0.0	0.0	0 • 0	
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0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	·•0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0									_
		RUW 52 .							•	
0.0	0-0-	0.0-	0.0	0.0	0.6	0.0	0.0	0.0	0.0	
0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0. 0	0.0	0.0	0.0	0.0	
0·•0			0.0	0.0	0.0	0.0	1:16400-08-	-2.05080-10	0.0	
-4.01250 04	4.59995 10		635D 08	-2.05080 10	0.0	0.0	0.0	0.0	0.0	
0.•.0	υ• G	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0		0.0	0.0	0.0		0.0	0.0	0.0	
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		RDW 53.	•							
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0.0	C • O	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 • 0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-5.8980D 07	
C.* 0	0.0	1.17960 08		0.0	-5.89800 07	0.0	0.0	0.0	0.0	72 -19
00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	٠ ٥•٥	0.0	· · 0	. 0.0	0.0	0.0	. 0.0	0.0	0.0	30
6.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 • 0	
0 • 0	c • c		•	*			· · · ·		· .	
		•••ROW 54								

		: (- V.	= 1	3.00	0.0	c c			0	0.0			•
		0.0	0 (•	o	0.0	0.0	0.0	0.0		0	0 1 0	:	٠.	
		0.0	0.0	0.0	0	0 • 0		0.0	0.0		0.0	0.0		tion is desired an interest of the contract of	
0.0		0.0	0•0	0.0		0.0	0.0	0.0	0.0		0.0	0.0		•	
1-	-1 - 38 Z C D C Z	-1-1635D_08	0.0	2.	2.1.740D_07-	-4.61250-0	0.0-40	-1.087.0D	-071-64	8000	0.0	0.0	0		
0.0		. 0.0	0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	0		
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0 • 0		0.0	0.0	0.0		0.0	0.0	0.0	0.0	·. ·	0.0	0 • 0	0		.
0.0		-0.0													
			•••ROW 55	20						· ·					
0.0		0.0	0.0	0.0	0	0.0	0.0	0.0	0.0		0.0	0.0	6		
0.0		0.0	0.0	0.0	c	0.0	0.0	0.0	0.0		0.0	0.0		-	-
0.0		0.0	0.0	0.0	0	0.0	0.0	0.0	0.0		. 0.0	0.0	0		
0.0	2	0.0	0.0	0.0	0	0.0	0.0	0.0	0.0		0.0	0.0	,		
0.0		0.0	0.0	0.0	0	0.0	0.0	0.0	0.0		0.0	0.0			
1.1	1.1640C CB	-2.050AD 10	0.0	-4-	-4.61250 04	4.59990 1	υ•υ o	-1.16350	08 -2.05080	10	0.0	0		٠	
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0.0		0.0	0.0	0.0	0	0.0	0.0	0.0	0.0		0.0	0.0	0		
0.0		0.0		:			-, •			· .			•		
			ROW 56	9			-								
0.0		0.0	0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0			- 1
0	0	0.0	0.0	0.0	0	0.0	0.0	0.0	0.0		0.0	0.0			
0.0		0.0	0.0	0.0	0	0.0	0.0	0.0	0.0		0.0	0.0-			
0.0	•	0•0	0.0	0.0	0	0.0	0.0	0.0	0.0		0.0	0.0			
0-0	·	0.0	0.0	0.0	0	0.0	υ·0	0.0	0.0		0.0	0.0			- -
0.0		υ•υ	-5.8980C	0.0 70		0.0	2.92650	08.0.0	0.0		0.0	0.0	•	• • • • • • • • • • • • • • • • • • •	
0.0		0.0	0.0	0.0	0	-1-8100 <u>n</u> -0	0.0-8	υ•.0	0.0		5.2670	0-01-0-0			
0.0		0.0	0.0	0.0	o	0.0	0.0	0.0	0.0		0.0	0.0			,
C-0 O			0.0	0.0	0	0.0	0.0	0.0	0.0		0.0	0.0			
0.0		0.0		-											· · · ·
			NOW 67												
0.0		0.0	0.0	0.0	. · c	0.0	0.0	0.0	0.0		0.0	0.0			
0.0		0.0	0.0	0.0	. 0	0.0	0.0	0.0	0.0		0.0	0.0			
0.0		0.0	0.0	0.0	·	0.0	0.0	0.0	0.0	:	0.0	0.0		A-	0 R
0.0		0•ن	0.0	0.0	c	0.0	0.0	0.0	0.0		0.0	0.0			
0.0		0.0	0.0	0.0	c	0.0	0.0	0.0	0.0		0.0		•		
0.0		∵ 0	0.0	-1.	-1.08700 07	-1.16350 0	0.0	1.67530	08 -3.4309D	07	0.0	0.0	0		30
0.0		0.0	0.0	0.0	C	0.0	-1.48000	085.6240D	00 -1-00000	0.4	0.0	3-3-	8. 5500E 06		
89	8.2000D C7	0.0	0.0	0.0	c	0.0	0.0	0.0	0.0		0.0	0.0			
0.0	(0.0	0.0	0.0	0	0.0	0.0	0.0	0.0		٥٠٠	0.0	(
0.0	0	0.0				-							-		

0,0	0 0	0.0	0.0	0*0	0.0	0*0	0.0	0 • 0	ດ•o	
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200	0 0	0.0		· . '	! -	0.0	0.0	0.0	0.0	
4	0.0	0.0	- 600-	0-1090500-280		0000 0000	0-7	0.0	-6.2090D 07	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
7.0		•••ROW 59	•••						manifestation and the contract of the contract	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 • 0	
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 • 0	
·• 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0 0	0.0	0 0	0 0	0 0	0 0	0.0	0 0			
0.0	-1.00000 06	1	0.0	0.0	0.0	0-0	0.0	0 00000		
0.0			0.0	0.0	0.0	0.0	0.0	0 0		
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0								_	
		•••ROW 60		ç		•				
. 0	0	0	0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	ŭ.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0		0.0	0.0	0.0		0.0	0.0	0.0		
٥٠٥	C .	0.0		0.0	· · · · · · · · · · · · · · · · · · ·	0•0	. 0.0	0.0	2.00000 06	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	.0 • 0.	N P
	and the state of t	ROW 61	•	the state of the s	man mer enter out tot of the company of the foreign		Andreas de la company de la co		A A STATE OF THE PARTY OF THE P	812 age
0.0	0.0	0.0	. 0•0	0.0	0.0	0.0	0.0	0.0	0•0	: !OR ! A
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	72
0.0	0.0	0.0	0.0	0.0		0.0 .	0.0	0.0	0.0	-0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 • 0	0.0	0.0	30
0.0	0.0	0.0	U* 0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0 8.05000 67	c c	0.0			C 0	0.0	0.0	0.0	1.10000 07	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	***************************************

	υ• 0	ROW62			the difference on another description					a calcagado, no de unhástico e na o desercios	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
	0.0	0.0	0.0	0.0	C • O	0.0	0 6		0.0	0.0		
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0		
0.0	0 • 0	0.0	0.0	0.0	0 • O	0.0	0.0		0.0	0.0		
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0		
C.0			0.0	, 0.0	!	0.0	0.0		-1-0000p0	0.09		
0.0	8.10000 07	0.0	0.0	-8.00000 07	0.0 70	0 0	0 0		0.0	0.0		,- -
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-	0.0	0.0		
J. O	0.0	KOW 63										
0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0		the same management in the same of
0.0	. 0 • 6	0.0	0.0	0.0	0:0	0.0	0.0	•	0.0	0.0		
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	٥٠٥		
0.0	. 0.0	0.0	٥٠٥	0.0	0.0	0.0	0.0	.,	0.0	0.0		
00	0	0.0	0.0	0.0	٥•٥	0.0	0.0	•	0.0	0.0		
0.0	0.0	0.0	- 1	·-	0.0	0.0	0.0		0.0	-2.00000	0 06	
-1.10066 67	0•0	5.4000E. 06		B.C.	0000	0.0 90	0.0		0.0	0.0		. ئى
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0		
၀•္	٠ •	0.0	0•0	0.0	0.0	0.0	0.0		0.0	0.0		-
0.0	0.0	e medit specialism i semblemba e e e e e em empera est e est tomo por		MAR OPENSAL PROPERTY OF THE PR	No					to the chart property on the property of the second		
	· ·	KOW . 64	•									<u> </u>
0.0	0.0	0.0	0.0	0.0	0 • U	0.0	0.0		0.0	0.0		
0•0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0		
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0		
0.0	0.00	9.0	0.0	0.0			0		0.0	0 • 0		
0.0	0.0	0.0	0.0	0.0	. 0.0	0.0	0.0		0.0	0.0		
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4 • 23e5C- C7	0.0	3.5500C-06	-3.9000D-07-	0.0	0.0	0.0	0.0	···· 0 • 0 ····	0 • 0	
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٠.	÷	ROW 72 .	•		•		•		÷.	
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	0.0	0.0			0.0	0.0	0.0	0.0	0.0	
०•०	. 0	0.0	0.0	0.0	. O • O	0.0	0.0	0.0		
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		١.	0.0	1	0.0	0.0	0.0	-2.26300-07-	0.0	
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	90 0008 · 8	ĺ	0.0	-5.33000 06	5.90000 07	0.0	0.0	0.0		T
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У.;	0.0	0.0	0.0	0.0	0•0	0.0	0.0	0.0		<u>-</u>
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	0.0	0.0	:	0.0	0.0	0.0	0.0	3.90000 07		<u> </u>
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	ROW 75	•								<u>;</u>
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0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
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-3.20200		.	3.45400 07	0.0	0.0	-2.5200D 06	· .]	0.0		: ; .
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	ROW 76 .									:
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•	ROW 77	•								

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. 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0•0	0.0	0.0	0.0	0.0	0.0	,
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		RUW 78			•			-	A Administration of the Control of t	•
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	O. 6.0	0.0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	030
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ניינו	0 0									

		. 13 %OH.					- · · · · · · · · · · · · · · · · · · ·			
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6.0	v•0	0.0	i		0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
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2005	0.0 90	0.0	-3.5800D o	0.0 96	٥٠٥	0.0	0.0	0.0	0.0	
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(·•0	υ• ū	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
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0.0	J.0.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
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0	0.0	-0.0-	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	C • O	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-
0.0	ں • ں	-0.0	0.0	0·0	0.0	0.0	0.0	-2.82000-0	7 -4.92310 08	
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(0 0 -)	Ü.Ü.	0.0	0.0	0:0	0.0	0.0	0.0	0.0	0.0	
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	many d m cum manne , decrease a debit to man advisore	•••RUW 85							A COMMISSION OF THE PROPERTY O	
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0.0	Ú•0	0.0	0.0) 	0.0	0.0	0.0	0.0	0.0	~ —
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0.0	-4.2300D 07	-7.38520	0.0 80	9.87100 07	2.46380 08	0.0	-5.64100 0	7 9.84900 08	0.0	
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0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
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C•3	: 0•0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0*0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0.	0.0	0.0	
C•0		0.0	-3.9300D 0	6 0.0	0.0	3.94780 06	0.0	0.0	-1.7800D 04	
C • 0	٥.0						•			
		•••ROW BB	• •					•		72 -28
0-	ن.• ن	0.0	0.0	0.0	0.0-	0.0	0.0	0.0	0 • 0	
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	0.0	0.0	0.0	0.0	0.0	0.0-	. 0.0	0.0	0 ° 0	
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... MODE SHAPE... COPRESPONDING TO NATURAL FREQUENCY

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3.3059D 00 CYC./SEC. ... MODE SHAPE ... CORRESPONDING TO NATURAL FREQUENCY -1.17910-05 -1.02520-05

4.0383D-04 -1.1844C-05 6.13810-04 4.3 FO BD-04 -1.180 4D-05 Aministry 2.77790-04 -1.17460-05 1.12660-01 -1-17971-05 4.34150-04 3.95210-04 -1.1779D-05 1.1311P-03 -1.15640-05 (4 -1.1792D-05 9 •80¢90-02 -1-17999-05

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		MODESHAPECORRESPONDING.INNATURAL.EREQUENCY6.94690-00-CYC./SEC.	-3.48070-04 -4-20-20-20-20-5.84280-05 -3.40780-04	4.69130-02	-9.42030-04 45000000 -7.659620-02 -9.42630-04 -3.55470-04 -19000000000000000000000000000000000000	1.32770-03 -3.64HBD-04 - 100 100 100 100 100 100 100 100 100 1	1.44640-03 -3.73300-04 -5.53360-02	-2.6C05C-06 -3.6665C-04	SOUTH SEASON	Transfer 1 . 96670-03		1.13060 01 CYC./SEC.	3.87080-05	1	2	2.8694E-04	1+06846-022+89118-047+13576-061+71630-022+89730-047+16610-062+24930-022+88850-047+52240-061+81800-03	-7-1704E-06	
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4 6.35680-06	6—4.44 psyconomics 27.7.4.K.	URAL-F.CEQUFN(1.22080-04 -3.39880-04 1.51240-02 -3.48070-04	A MARKETHAN COLORS	30 3.61540-0	3 -3.64885-0	4 Semilerations 2	3 1.44810-03	1.74310-03	1.98360-03 -3.69360-04	-	MIDE SHAPECORRESPONDING TO NATURAL FREQUENCY	5 -6.26740-00	3-5-6-6050-0		4 -7.07360-06	62-24930-0	2 2.8E26D-04	23.0372D-0
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6-23600-06	PV 55	MODESH A? &	-3.21340-04 -3.50420-04	Same and a second	-9.42635-04	-3.64280-04	A description of the Control of the	i	1.70830-03	1 -3.6897D-04		MODE SHAPE	5.07400-08 -6.94140-06 -2.91920-03	5-8:1050-06 -1-01090-03		-7.04200-06	1.71630-02	2-93370-04	3.00430-04
		-	1.5502C-06 -3.2142C-04	-3.5033C-04	-7-5962U-02	€ 1.308€E-03	-3.6604C-04	-4.7188L-02	T Winds	34 Action 1 6 6 4 4 C - 03 - 3 6 B 9 7 D - 04		•	5.0740C-08		50-36-36-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-6-	2.80430-04	7.13670-06	1.32400-03	3 • 6 3 5 8 C = 0 5
6.97266m.cc0.61.34D=02=8.36760=06 5.53750=06	1.70010-03	A:10	4.00556-05 -3.54110-06 1.55026-06 -3.21340-04 -3.37410-03	-6.26670-02 -1.50320-03 -3.50336-04 -3-369999486 -6.18840-04	A Semantide State of the Paris Paris	-3.6401U-04	C2. Zambarana 1.39080-03 -2.66040-04	2.11c0b-03 -3.66875-04 -4.7188L-02	1.50796-03 -3.66840-04 Transpose 1 .70836-03 -3.66930-04	ì	Ħ		3.24560-02	-2.004ct-03	1-S4640-02	-7.02795-Co -4.50080-03 2.8043E-04 -7.0420D-06 -1.7383-01	2.89118-04	5.6374[-04 -7.17950-06 1.3240C-03	7-7-17570-06
5.53750-06	1.7c01D-03		4.00550-05 -11-23334-02	-6.20675-02	-9.42050-04	-3.64010-04	S. E. Z. Bild C. S. C.	2.11000-03	1.50796-03	-3.06460-04	4.01675-01	Marine of the section	3.03176-07	-2-00-40-03 -5-85270-03	-2	-7.0279C-Co	1-0624F-02	5.63741-04	4 0-100000-2-

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6.24100-06

PO-UNEOF C Registrations

V. 206.11-02

60-14720-06

5.32270-06 ** Particulation -1.23180-04

3.74390-03 -5.27020-05 -2.32780-04 9.51330-03 2.71600-03 -7.56760-05 3.51160-07 -2.35405-04 -1.77215-03 2.5554L-03 -5.945ID-05 -2.340IE-04 1.2955D-03 -6.6749D-05 -2.352ID-04 -1.6692D-04 -7.4587D-06 -2.4933E-04 4.8721C-03 -6.32830-05 -2.3580h-94 -4.37540-03 -1.34400-04 -2.36060-04:-7.52780-03:-1.42160-04 -2.38740-04 -1.32400-02 -5.2075D-04 4.75240-03 -4.65160-05 -2.31540-04 9.70910-05 -2.36140-01 7.1279C-02 -3.56030-03 -2.11770-04 3.6792C-03 6.50780-03 -9.46220-05 -2.35530-04 5.22210-03 +4.33076-05 +2.30290-04 40-0423c-04 -6-1874D-04 -2.29726-04 -3.9000-03

77 84 37190-67 7-2,22360-04 74-2,17700-07 -1,02376-05 3,65076-02 -1,59080-05 73,70200-05 73,77440-05 -1,03640-05 774

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... MODE SHAPE... COPPESPONDING TO NATURAL FREQUENCY

1.53859 01 CYC./SEC.

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4.0940C-04 -1.3125C-05

9.20820-02

3.85320-04 -7.35570-06

7.82250-02

3.6132D-04 -7.3264D-06

6.52100-02

-1.51150-01---

1.74370-01. 6.11870-04 -1.92030-04 1.80500-01 -9.29640-03 -1.50820-04

3.03025-04 -1.9215D-04

1.65460-01

-1.50960-04

6.34860-02

6.11720-04 -1.5454C-04 -1.8920D-04 -7.7762D-03

-1.4328D-06 -1.9438D-04

-1.55960-03

1.2361D 01 CYC./SEC.

...MODE SHAPE ... CORPESPONDING TO NATURAL FREQUENCY

7.12790-02

-9.38370-03 -1.85040-04 5.67130-02 -2.54500-03 -1.98910-04 1.74580-02 -1.80180-03 2.35750-01

30	8.42101-04 6.05910-04 8.2375F-03 -8.77980-04 6.02100-04 -2.57410-02 -8.66350-04 1.97730-06 5.5885C-04 -7.2755C-02
	-1. +7836-02 -9.78928-04 5.84806-04 -3.71820-02 -9.32890-04 5.98158-04 -5.83070-02 -8.66216-04 8.02776-04 4.11256-03
	5.3732L-04 4.371AD-02 -1.0005L-03 5.4351D-04 3.187FD-02 -1.0074D-03 5.5746D-04 8.4007D-03 -1.0038D-03 5.7123D-04
	6.18256-03 -1.36390-01 -7.88765-02 6.48255-03 3.39090-04 7.88845-02 -2.08300-04 4.38295-04 6.33405-02 -6.63865-04
120 ge	-1.55046-01 -5.07950-03 8.53946-05 -1.44900-01 6.14010-03 1.95400-04 -3.83500-04 5.53110-03 1.36616-01 -7.88760-02
	-1.2041C+01 -1.71030-04 2.8E61C-04 8.57060-05 1.26540-02 -1.5398C-01 1.0984D-04 +1.2501C+01 -4.9688C-03 1.0385C-04
	-2.22070-06 2.26810-03 2.1606C-07 2.84570-04 -1.21690-01 -4.92920-04 1.64370-04 -1.26720-01 -1.70930-04 1.58440-04
	MODE SHAPECOPRESPONDING TO NATURAL FREQUENCY 2.6282D 01 CYC./SEC.
	1.30066-04 -7.95168-02 -2.4504E-03 1.8283B-04 -1.6508B-01 -2.6242E-03 1.7906B-04 -2.6148E-01 -2.6576E-03 -7.0121B-04
	5.22796-03 1.97790-04 7.06166-02 2.73950-04 1.96940-04 7.87250-02 3.58650-04 3.74930-06 1.96170-04 9.76216-02
	42.26930-044.
	1.0656D-02 8.789HC-04 1.8302D-04 2.1691D-02
	-1.25228D-01 1.5106D-03 1.366CD-04 -9.1960D-02 1.6312D-03 6.2857D-02 -1.0884D-
	1.052612012.60220204_1.05622504_1.216002041.06116_023.771.69=021.2260-041.05826-01-2.47550-031.22656-04
	-1.6301C-06 -5.0060D-03 4.7162D-07 1.0961D-04 -1.1118D-01 4.2800D-04 1.1854D-04 -1.0607D-01 2.6026D-04 1.1896D-04
	-2.6903D-04MODE SHAPECORRESPONDING TO NATURAL FREQUENCY 1.91060 01 CYC./SEC.
	-2.75750-03 -8.52610-05 41.67195-06 1.17390-03 -1.49130-04 -1.74840-06 4.75420-03 -2.10630-04 -1.76800-06 7.54230-01
***************************************	-1.5002L-C7 -1.31865-03 2.7762F-05 -7.8361D-07 -1.2753D-02 7.9091C-06 -8.9627D-07 -7.1805D-03 -3.4052E-05 -1.4766D-06
	6.59956-06 -1.41180 02 3.76266-05 8.51570-08 -1.40930-02 4.05670-05 3.06630-08 2.89276-09 -1.37966-02 3.56450-05,
	3.50440-05 1.84 Apr-07 -1.41700-02 3.91660-05 1.15150-07 -1.40570-02 4.16340-05 3.70620-08 -1.57400-02 1.40150-06
	1.4 G60-05 3.16050-07 -1.44980-02 2.29570-05 2.43250-07 -1.43910-02 2.96210-05 2.43550-07 -1.42810-
	-1.2247L-04 -1.03330-05 -1.61HCD-02 -1.58C6D+04 5.47350-06 -1.6012D-02 -6.7896D-05 4.41230-06 -1.6631D-02 -9.6762D-05 2.0613D-06 -1.57880-03 1.27010-06 1.27010-06 -1.61670-03 6.01470-06 4.02660-03
	-5.48426-65. 7.20805-07 -1.50826-02 -1.62050-02 -1.51050-02 -1.63426-02 -1.62850-02 -6.00850-05 -1.04306-05 -1.63230-02
	-7.57260-05 1.0441D-06 -1.5927D-02 -6.184
÷ .	-1.14130-02 -1.14130-02 -1.14130-02
	.c4376-05-44.630105-03-7.2443C+05-1.e68420+05-7.21350+0
anderstell for state from systems for and an enderstand a south desire.	8.5.128D=063.604CD=061.5218C=051.4173C=
	* 6.61220-03 -1.05710-04 -1.50460-05 3.65200-03 -6.42250-05 -1.51830-05 1.70880-03 -1.05110-05 -1.66410-05 -1.43390-01
e esperante de la compansión de la compa	

	7

-6.3572F-04 6.00249-04 -7.9925E-C2 -3.66120-05 6.00920-04 -7.85510-02 8.8333D-05 6.0222D-04 -6.3155E-02 7.6503E-04 6.0127L-04 -3.20280-02 1.0029E-03 5.9909R-04 4.8892N-03 5.966RD-04 4.3804D-02 1.1234D-03 -4.3376D-04

... MORE SHAPE ... CORDES PONDING TO NATURAL FREQUENCY

1.56440-01

2.768 9D 01 CYC./SEC.

	-1.74251-05 7.04306-91 2.80726-03 -1.77040-08 4.64840-01 9.7243F-63 -1.77740-05 4.99720-01 2.70326-03 2.12706-66
	1.13372-03 -1.50390-05 5.19830-02 2.41330-02 1.166670-05 1.12840-01 2.55920-03 -1.65170-05 2.69160-01 2.85360-03
	-7.9670D-05 7.5852D-02 -2.1408D-03 -2.2939D-05 -4.1796D-02 6.4508D-04 -
30	5.7380E-04 7.48680-05 -7.9508D-02 6.0145C-04 5.2321D-05 -6.5441D-02
	1
	-5.40400-04.
OR: A	4 4.29230-04 -5.49530-03 -2.34670-02 5.12790-04 4.34870-02 -6.43430-04
	-8.1639[-07 -2.99740-03 -3.1744L-08 4.1428D-04 6.89500-02 2.3324D-04 4.8897D-04 5.9585D-02 -1.0279D-03 4.5207D-04
	-4.02930-02 -6.88310-04 -3.57740-06 -4.68470-02 -8.05860-04 -3.18470-06 -4.65510-02 -9.14360-04 -3.07860-06 7.01170-03
TO A TO A STATE OF THE STATE OF	- 1
	3.6509E-021.26730-045.67120-064.24760-022.51120-054.16860-062.30660-01
man resent dies dies des des des des des des des des des d	
	-1.37400-05 5.8360E-02 -1.3153D-03 -7.26600-05 8.11920-02 -7.79680-04 -
	5u-denes • ieo-gene
	-2.3463D-04 7.40N9D-06 1.3903E-09 9.7926E-02 -2.016ND-03 7.6841E-06 1.0998D-01 -1.6126D-03 3.3928D-05 1.1047D-01
-	-Z.51955-01*MODE SHAPECORPESPONDING TO NATURAL FREQUENCY 4.73060 01 CYC./SEC.
	2.03y3L-04 1.99771D-01 -8.5667C-04 2.0467N-04 1.5674N-01 -1.0688D-03 2.0435D-04 1.1815D-01 -1.1232C-03 -5.9913D-05
aman i a se sa e a aman papa pentu, apaga e ada papaga da an sa ingalag	1.95206-03 1.97810-04 1.81316-01 1.09640-03 1.98450-04 2.04000-01 8.54580-04 2.02030-04 2.12576-01 -3.71730-64
The same of the sa	
	1.8698E-04 6.6508D-02 1.8749D-03 1.9612D-04 1.0409D-01 2.1885D-03 3.7075E-04 -
× ·	# 1 - 54 700-04 - 2 - 74 24 0-02 1 - 24 360-03 1 - 58 920 - 03 1 - 58 93 00 - 03 1 - 58 93 00 - 03 1 - 58 93 00 - 04 1 - 58 93 00 - 03 1 - 58 93 00 - 03 1 - 58 93 00 - 03 1 - 58 93 00 - 04 1 - 58 93 00 - 05
	*36545-03 -5.74528-04 -
and the same of th	ł
	-1-30000-05
and de se	
	-1.7177L-04 3.8617D-04 -2.8560C-02 2.8948D-05 3.8673D-04 -3.7333D-02 6.9348D-05 3.8853C-04 -3.0861C-02 2.5275D-04
tenan van e ra op in andiperem kan den derkage "op de epid en de kankler of the de dektyden yn.	~~~20-03-03-03-03-03-03-03-03-03-03-03-03-03
	5.3612D-04 -
*	į
	2.4 - 40-12640.
	90-019-1-9- KO-029KV-6

		•							
5.4641D 01 CYC./SFC.		-3.6699D-03 -1.1206D-02 1.5503D-04 4.4617D-02 -6.4915D-04 1.6058D-04		1.4530N-04 -7.3424D-02 -2.6206D-04 1.0856D-04 -4.7046C-02 2.9075C-04	7.1642D-05_11.5576D-02_5.1636E-04_6.8982D-05_7.9343D=03_5.0783E-04_6.2733D-05_7.1127E-03_4.5311E-04-5.6396D-65	1.9091D-04 4.3491E-05 3.6506E-02 -1.2904P-05 -5.2905E-04 -4.9378D-02		4.4904D-05 -8.5170D-02 -2.9208D-03 4.7583D-05 -2.0444D-01 -3.7583D-03	4*919£fir@5342£589r013*8923Er035*00910r05_=4*74240-013*87300r035*63370-05_46*09030-013*865£0-03-45*43140-06
AL FREQUENCY	-1-4-32-8D-04	1.55030-04	8.E.050D=02_=	-2.6.206D-04	6 - 2.7330-05-	3.65060-02 -	-1-75420-05	-2.92080-03	-5.4 C-3.3.7D=05=
* MODE SHAPF CORPESPONDING TO NATURAL FREQUENCY	1-48570-04-	-1.12060-02	1.36360=04	-7.34240-02	5.07830-04	4.34910-05	-3.8C36P-02-	-8.5170D-02 -	-3-87300-03
• • CORPESPOND	8.06010-02-	-3.66990-03	4.46350-04	1.45300-04	-7.934.3D=03	1.90910-04	4.1.2010-05-	4.49040-05	=4-7424D-01-
*MODE SHAPF.	1.01910-04	1.31275-04	5.49410-02	5.66510-03	_6.8982D=05	3.06890-02	-1+3765D+03-	-2.60420-03	5.009.10-05
•	-3-5483C-08	1.03535-04	1.25210-04	5.66510-03 -5.48090-03 9.44530-02 5.66510-03	_5.1.636C-04_	2.03b3b-02 3.4703b-04 4.9579b+05 3.0589b-02	-3.249el-02-	-6.37956-64 4.45065-05 -1.6668CE-62 -2.6042D-03	-3. E933C-03
·.	3.20500-03	5.08966-02 -1.47356-03 1.03536-04	-1.50760-04	-5.48090-03	=1.557.6D-02	3.47030-04	-3.4268D-0.5	4.45065-05	-3.32585-01
	-1,3250L=C7_	5.08965-02	4.172cu-02	5.66510-03	7.16420-05	2.03030-02	-=1.7105L-03-	-6.37950-64	4.919.50-05

	1	1							
•	•••	MODE. SHARE	••••CORRESPOND	ING_TO_NAT.UR	AL_EREQUENCY	6.25260	0.1- CYC./SEC	•••CORRESPONDING_IO_NATURAL_EREQUENCY6.2526D_01. CYC./SEC	
1.71110-06	-6.28000-05 -1.71110-06 3.02050-10 4.58380-02	4.58380-02	-7.43210-04	3-67750-06	•	-4.79710-04	2.32630-05	2.32630-05 6.95790-02	
-2.05.97L-04. 2.32760-05	4.68010-02	4.68015-02 5.42260-02	4.67070-02	5.66165-02	4.67070-02 5.66165-02 7.76165-02 -1.93680-04	-1.93680-04	4.29700-07	4.29705-07 7.78330-02	
5.19610-16	-2.02410-04 -5.19610-16 5.31100-02 -2.5829D-04	-2.5829D-04	-9-36130-05		2.67990-02 -3.65930-05 -3.58230-05	-3.58230-05	1.43950-01	1.43950-01 -3.52140-05	
1.43470-01	4.33356-05 1.43470-01 -3.52146-05 4.33356-05	05 4.33350-05	-7.70630-03	1.32240-04	-7.70630-03 1.3224D-04 3.55510-06 -3.89870-02	-3.8587D-02	D-02 1.64630-04 8.84600-0	1.6463C-04 8.8460C-07	
1.62580-04	-7.01810-02 1.62588-04 -1.8487L-06 -7.19760-02	-7.19760-02	1.36740-04	-1.933PD-06	-7.58950-02	1.3674P-04 -1.933PD-06 -7.5895D-02 8.7153D-05 -2.0102D-06 -7.5674D-02	-2.01020-06	-7.5674C-02	
1.97760-06	3.42180-05 -1.9776n-06 -8.33050-02 -1.71270-05	-1.71270-0E	-1-82950-06	12950-06 -8.67800-02	-6.3 FH4D-05	-1.6295D-06 -8.67800-02 -6.28840-05 -1.56520-06 2.1325D-01 -3.85290-05	2.13250-01	-3.86250-05	
8.40750-02	-1.17550-C0 -8.40750-02 -1.6135F-05 -1.5749R-07	-1.57490-07		-6.5886C-06	-1.52360-06	-8.74440-02 +6.58866-06 -1.52360-06 6.83530-09 -8.76825-02 -8.76215-05	-e-7682C-02	-8.7621C-05	
8.95490-02	-9.70820-C7 -8.95490-02 -8.2506E-05 1.20900-06	-8.9549D-02 -8.2506E-05 1.2090D-06		-9.0642D-02 -4.8729D-05	1.62870-06	1.62870-06 -9.82680-02 4.14740-05 3.43880-06	4.14745-05	4-14746-05 3-43886-06	

MODE SHAPECORRESPONDING TO NATURAL FREQUENCY 6.66870 01 CYC./SEC.	ECOPRES PONDING TO NATURAL FREQUENCY 6.66870 01 CYC./SEC. 1 -2.36990-11 -5.86840-14 -1.17840-11 -2.47970-11 -7.01420-14 -1.2000-11	6.66870 01 CYC./SEC.
**************************************	E 5-5-1-1-0-12-11-1-1-1-1-1-1-1-1-1-1-1-1-1	11-2002-11 -1-0210-11 11-0200-11

4.21090-06

4.60680-04

3.1456D-04 4.16310-06 -1.0646D-01

1.71930-04 7 3.58860-06 -1.05600-01

-1.02930-01

-1.226CD-04

2 - 5	9.1355(-03 -2.20040-03 -1.76826-04 -1.46940-05 -7.20040-04 (1.46940-05 -0.69440-05 - 46440-05 -1.46940-05 -1.46940-05
: 72 -36	1.03950-07 -1.33470-03 -1.32240-08 -1.71600-04 5.39780-02 2.14370-05 -1.24010-04 3.14700-02 -2.22750-03 -1.21390-04
120R ge A	MODE SHAPE COPRESPONDING TO NATURAL FREQUENCY 7.4851D 01 CYC./SEC.
N8 Pa	-1.1081C-11 -7.9876D-12 4.1734C-14 -1.0295D-11 -5.8590D-12 2.5324D-14 -1.3484D-11 -5.9172D-12 -5.8265D-14 -1.1620C-11
•	6.865VC-14 -1.18370-11 -1.6123C-12 -5.38R2D-14 -1.1R240-11 -3.8099C-12 -4.39600-14 -3.5178D-16 -1.1749C-11 -6.5751D-12
-	34-66264-1-25-67090-141-17486-114-40730-124-74900-141-1-18000-1-15-46730-124-38170-141-15970-11-1-79950-12
•	-1.16570-11 -1.58690-13 -5.36806-14 -1.16610-11 -8.22610-13 -5.57986-14 -1.16690-11 -2.08020-12 -5.55940-14 -1.16980-11
• .	-1.72750-11 1.36310-12 -1.20386-11 -7.63050-12 3.92210-13 -9.75160-12 -1.57680-12 2.86920-13 -4.55030-11 -4.21480-02
	2+526±0±117.0056D=14_=1-2157b=11_=1-1502D=11_=1-06870=11_=2+12020=111-1-1-1330=112+53230=1
	-1.1004L-11 -5.11671-12 2.1/866-16 -1.21160-11 -2.36090-11 -5.86840-14 -1.17840-11 -2.47976-11 -7.01420-14 -1.20020-11

9.66748-04 -3.87788-05 -4.95228-02 1.77888-04 -1.09678-05

1.81850-n1 -2.91440-03

1.86310-05

3.40666-03 -1.11446-03 2.10420-01 -2.8099C-03

9.0674U-04 1.60796-05 3.43000-05 -1.46790-02. 2.87270-04. 3.49940-05

-2.355550-03

5.21756-02 -3.34706-03 3.02776-05 -2.13870-02 -3.56990-03

3.4012P-05 -9.5354P-02 -3.7875P-03 -3.4365P-05 -8.7625D-02 4.98359-02 +3.40190-03 +1.44860-05 3.445520-05 +1.73100-01

1.2021D-01 -3.1241D-03

2.25770-05

9.01685-02 -4.49335-04

4.72100-02 -1.65700-02 -2.33660-03	-1.3816L-04 9.63249-07 -5.7259D-10 1.9544D-01 4.0934D-03 3.31840-05 5.4293D-02 2.1781D-03 -2.1398D-04 4.7 -1.3816L-04 9.63249-07 -5.7259D-10 1.9544D-01 4.0934D-03 3.31840-05 5.4293D-02 2.1781D-03 -2.1398D-04 4.7 -1.1276D-03 1.3374D-06 2.2260G-02 -1.2504D-03 -9.7206D-05 6.3552D-02 -1.3003D-03 -4.1832D-05 -1.6529D-01 -2.3 -1.1276D-03 1.3374D-06 2.2260G-03 -1.2504D-05 -9.7206D-05 6.3552D-02 -1.3003D-03 -4.1832D-05 -1.6529D-01 -2.3
	MUDE SHAPECOPRESPONDING TO NATURAL FREQUENCY 8.70080
1.3292D-02 2.7809C-C4 5.8110D-05	1.5572D-04 -9.4967D-04 -1.7824E-02 -4.9429D-05 -9.7368D-04 -1.9500E-02 -1.0489E-05 -1.1537D-03 -1.4770E-02 -1.2605E-03 -2.5884ED-03 3.5275E-04 -1.3347D-03 1.1651D-02 4.4233E-04 -1.3603D-03 2.7380D-02 4.5745E-04
2.5996D-03 6.0933C-04 5.5841D-04	1.6506D-02 1.9032C-04 -3.1935D-04 1.6453D-02 9.651CD-05 -4.6512D-04 1.2832D-02 -3.8965C-051.2772D-04 -7.5147C-04 -1.1765D-02 -1.6749D-04 -8.9108D-04 -9.2275D-03 -1.5762D-04 5.5764D-04 -
1.0703D-03, -6.0028D-04 1.2745D-01	1.3877P-02 3.7676P-03 1.5027F-02
9.34070-06	
-1.16870-62 -0.7058D-03	1.3413D-04 -2.2771D-03 -3.8346D-04 -1.0911D-04 1.46510D-024.2793D-041.2618D-061.3659D-04 1.7464D-02 -3.0528D-05 1.6760D-04 -1.1667D-02 5.4850D-04 1.63450-04 4
-2.8847C-03	2.1120C-02
3.85670-04 5.5019D-05	
•5%520+06	2- 20-0501-1 10-0560v*S 50-0089)**, F0-11080*V 10-08040*8 30-09200*V,

•	5.0646L-07 2.02330-09 4.6559C-12 -3.6714D-02 -9.4640D-05 -4.5231D-07 6.6103D-04 8.4856D-05 2.4943D-05 8.6642D-04
30	MODF SHAPECORRESPONDING TO NATURAL FREQUENCY 1.55870 02 CYC./SEC.
	2.0556C-05 -2.72830-01 6.6525C-03 3.12130-05 1.16910-02 9.4985C-03 3.21690-05 3.6132C-01 1.0451C-02 -5.1C90D-07
3120 age	5.53770-06
	1.12080-01 1.21450-03 -3.95180-06 1.13860-01 1.34360-03 -1.
THE STREET WAS A STREET OF THE PARTY AND A RESERVE AND A STREET AS A STREET, WHEN A STREET	
	-04 3.6068D-05 -7.2751D-04 -1.5077D-04 -7.2580C-06 1.5549D-
	43.57200-065.50560-
	-7.48E5D-09 -2.6352D-04 2.6352C-11 2.6030D-05 -1.0739D-04 8.8049F-06 5.0610D-05 1.8562D-04 2.8898E-05 5.1368D-05
	MODE SHAPECOFRESPONDING TO NATURAL FREQUENCY 1.38450 02 CYC./SEÇ.
	.039ep-1
	-3.2514b-13 5.4724f-12 3.86335-12 4.2634D-12 9.5327D-12 1.3553D-10 4.7624D-12 6.7632D-11 2.0828D-10 -8.0759D-13
	4-40735-11
	-11 -6.9
•	-1.32586-12 -5.3522D-12 -6.7507D-14 -1.46956-12 6.4403D-13 1.68776-13 -7.56126-12 -2.
	-4.68319-12 -2.21256-12 -3.62330-13 -1.97590-12 3.04
	TO A A A A A A A A A A A A A A A A A A A
	2.0558U-02
	• 924 0D=037 • 1638D=0
	1.45720-04 2.72560-01 3.08800-03 2.14860-04 2.81765-01 -2.63
	1.22455-04-
	3.0548D-0.12.8254E-035.5725D-062.1454D-012.5952D-034.
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-1.91789-04 3.36940-08	-3.5676h-02 7.5739b-02	7.32890-08	SHAPE CORNES PONDING	-8.4658h-05	-2.94790-04-	-9-3602N-05	1.35910-02	5.89280-04	-1.07-780-05	.94360	11.40.00	••••MODE…SHAPF:•••CORPESPONJING.TO.NATURAL—FREQUENCY 0 -9•91400-03 -1•87960-02 -2•73870-05 5-32070-02		-4.46790-02	-1.42500-02	-1.83320-03	3.82835-06	1.63200-03	1.05980-03	-3.89480-06	-	SHAPE COPRES POND ING	-4.4723D-06	-4 :2 8550 -05-	\boldsymbol{c} :	-8-45620-07-	4.64090-02	1.83010-03-	9.67620-08	6.87115-08-	-4-25685-02	
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-2.401cf-07 -1.4657p-09 -1.1652p-09 3.1623p-03 5.7055p-02 -2.2172p-05 -2.2511D-02 -2.6463p-01 1.1862p-01 -2.4342p-02

... MODE SHAPE ... CORRESPONDING TO NATURAL FREQUENCY

2.6215D 02 CYC./SEC.

	-4.2460C-27-2.66840-03-9.5712C-06-5.05010-073.01449-03-5.42820C-06-7.00340-071.7302D-03-1.2781C-05-1.2293D-C6
72-030 ·40	5.86890-05 2.2810C-06 4.36630-02 1.14150-04 2.00170-06 3.44020-02 1.7398C-04 9.8618C-07 2.3400C
N8120R: Page A	1.63845-06 2.77865-09 -4.51015-10 -3.26075-92 3.49745-02 1.35165-05 5.89615-01 -2.70765-01 1.67715-02 5.93785-01 = 2.257865-01 1.67715-02 5.93785-01 = 2.257865-01 1.67715-02 5.93785-01 = 2.257865-01 = 2.257865-01 = 2.46955-01 = 2.46955-01 = 2.46955-01 = 2.46955-02 = 2.46715-62
	.729ED-10 MODE SHAPECORRESPONDING TO NATURAL FREQUENCY 3.2628D 02 CYC./SEC.
	5029U-03 -0.FABSD-07 -3.2871C-09 1.746AD-02 -7.1561D-07 1.9584C-08 2.5520D-02 1.7690n-07 3.1311C-08 -7.7
	7.10/CD-11
	1.24858-07 9.62158-02 -9.05268-06 1.17548-07 -1.89528-02 4.81648-07 4.17538-08 1.78378-03 -6.4
	-1.35270-05 6.60550-08 3.9534D-01 -1.69150-05 7.42070-08
	80-03 -1.87240-03 5.69650-03 -1.
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-	-5.65905-11 4.75710-11 5.58070-03 -3.32840-03 -7.53340-07 -6.9103D-02 2.30
-	.07176-65
	EC-02 -2.1557C-
	1.03030-06
	1.4560C+011.2714C+024.6772D+063.0858D+017.3036C+033.
	-2.9228D+05 -1.5145C-04 -1.0796D+06 -5.0139D-06 2.1262D-03 -2.5352D+04 -5.9435C+06 -5.6044D-02 7.3126D-

	14544D=1111.00A0D=063.0900C=125.1482D=071.1881D=042.0120C+067.8436D=056.8733D=041.2531D=047.9684D=05
	MODE SHAPECORPESPONDING TO NATURAL FREQUENCY 2.8233D 02 CYC./SEC.
-	4.69485-05 -4.05165-07 2.27785-04 3.24270-04 -4.33180-
	*EE53D-06 -9.9755D-08 -2.4300D-04 -6.4
	1.76560-06 4.0854C-04 1.01960-04 -1.58170-06 -2.
	-03 3.0001D-04 5.4950C-06 1.0271D-
	1.0847U-02 +3.8014U-02 5.2208D-04 3.0506D-03 -8.7747D-04 2.2844D-05 2.7449D-03 -4.235
	-0010H-F- F0-76961-1- F

3.33560 02 CYC./SFC.

***MODE SHAPE *** COPRESPONDING TO NATURAL FOR DURINGY

1.40×11-10 -4.05×00-05 8.092×0-14 ÷3.05490-06 -5.45×00-06 3.480×0× 6.69830-05 4.44630-05 -2.36890-06 6.12760-05 3.92526-05 -2.40990-06 -7.37690-06 1.11250-04 -9.48?70-06 -1.99910-05 4.57590-05 4.15740-05 +3.67950-08 4.22230-05	
4-19656-05 2.64090-07 4.6072E-05 7.46000-05 2.17400-06 2.6488E-05 5.25140-05 -4.97720-07 -2.96255-06 -6.9409D-06	The confidence of the same of
-4.04510-06 -6.54090-06 1.39290-08 -2.07950-06 4.16960-05 -6.72490-06	
2.6910D-06 5.7433D-03 4.1375D-04 2.1305D-06 7.1155D-03 1.5905C-04 1.4573C-0	-
0050(100 -3.63290-07 -2.4607(-07 -1.0025)-06 -3.25250-07 -6.005820-08 -1.70430-02 -2.17(60-04 9.39(30-05 0	,
74120-03 -1.47190-07 1.85310-01 5.91110-03 -1.67970-07 2.87430-01	
1 1.37325-02 1.53650-07 1.63755-01 2.43735-02 -3	
MODE SHAPE CORRESPONDING TO NATURAL FREQUENCY 3.47050 02 CYC./SFC.	
54-4591Lm.C72-91.200-097-7547p-10=1-2359Dm02-m6-8892Dm02-m4-3303D-052-6290D-01-m6-1263D-01-+2-4852D-022-6311D+01	
5.70366-01 -2.53190-02 -3.37966-02 4.63150-01 -3.07960-02 -2.47310-01 1.81670-01 5.81180-01 -5.63770-03 1.64610-01	
63450-0-1-488820-03-	
6-5105C-04 -1-5974D-02 -6-1716C-02 6-5105D-04 -6-8462D-03 -2-1099C-03 6-2190D-05 -4-7041D-04 -9-6156C-04 3-2132D-05	

-2.334£C-04 -2.4164D-06 1.5445C-03 -1.3636D-04 -9.3782D-08 -1.1785C-04 4.4373D-05 1.0358D-06 1.7200D-05 -2.7633D-07	***
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7.508AP-06 -1.30305-07 -1.65388-09 2.249AP-04 -3.61665-08 -3.4006P-10 -4.2665D-03 -2.5839D-08	
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-2.40356-15 -4.10728-02 -3.62346-12 -2.17858-12 -3.43818-02 -6.87408-11 -7.81918-13 -3.63538-12 1.55386-01 -9.99918-11	
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3.44100-01 -1.12930-11 -9.03270-13 -2.48330-01 -1.95290-11 4.34610-13 -6.16020-01 7.71720-12 1.05060-12 9.89300-04	* War A War
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-7.22700-C6---7.44710-08--8.380SC-05 -4.37170-06--6.34000-08--7.26130-07--2.5199D-08--2.0312D-08--5.4662D-08⁻-2.1739D-10

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-5.03960-04 -2.88100-05 -5.57835-06 -1.67050-03 -2.	.67050-03	-2-36550-07	36560-07 -6.77750-06 -5.88780-04 3.36290-05	-5.88780-04	3.36290-05	3.47490-05 4.45010-05	
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PONDING TO NATURAL	4.29540-08	4.64820-04	-1.4158C-04	-3.1350D-03	1.66710-04	-2.32150-08	-6.780ch-03	-6-02720-63	-1.2265C-04		ING TO NATU	7.661-PC-08	7.77280-04	-2+3-190C-04	-5.65400-03	6-4 E7 50-07	-3.8440D-08	-7.69950-03	4.01800-03	-8.0477D-05	;	POND-INGTONATURALF9EQUENCY	-9.4813D-06	3.90520-01
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	-4.35020-09 -	-1.81230-05		7.81450-06	-3.17250-02	-0.3453N-04 -	1.78870-08	6.44150-09	7.35869-04	<b>.</b>		60-021v9-c	-3.3611D-05 1.3566D-06	1-63570-05	1.32720-05	4.51110-02-	-3.4393D-93 -1.4655D+07 -2.4316D-01	<del>3</del> 0 0 5 0 2 5 2	9-66330-09 -2-25940-02 -2-47190-05	4-42330-04			3.02820-13	1.61930-02
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My will thank the -6-168301-03 N8120R: 72 Page A-45

-6.2190D-05 3.41490-08

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	MODE SHAPECORRESPONDING TO NATURAL FREQUENCY 9.1233D 02 CYC./SEC.
-	-3.91216-12 -1.98400-02 -2.13166-02 7.07016-12 -9.61020-02 2.68456-02 -3.91290-12 1.18220-01 -1.58170-02 8.35666-16 -1.53290-04
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	1.057AD-06 -1.193AE-07 1.399BD-05 1.9A01D-07 -9.4256E-07 -2.8E65JD-04 6.3326D-06 1.0464E-07 -1.0466BD-06 1.0464E-07 -1.0466BD-06 1.0464BD-07 -1.0466BD-07 8.0411E-07 1.7704D-08 3.2676D-09 7.2654E-04 -1.5427D-04 4.0083D-09 3.5193D-04
	2.62770-14 -4.81850-11 1.066820-15 -1.03060-08 3.81150-09 5.76930-08 -7.990640-09 -5.84090-06 -1.30240-07 -7.32540-10 1.34560-05 -1.93540-07 1.00630-09 1.16590-06 1.41900-07 4.72020-07 6.24470-09 -5.44900-09 1.16590-06 1.41900-07 6.244000-08 -5.44900-09 -5.4
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20R:	-1.2425L-02 2.5507D-11 2.9853D-02 -4.7435D-02 -1.3933D-11 4.8977L-03 2.2540D-04 1.9466D-12 -7.0523D-03 4.7052D-04 -1.7052D-04 1.9466D-12 -7.0523D-03 4.7052D-04 -1.7052D-04 1.9555D-03 4.7052D-04 1.9058D-03 4.7055D-05 15 17 15 15 15 15 15 15 15 15 15 15 15 15 15
	4.27150-02 1.54110-03 -1.01950-11 -1.70090-01 -1.10140-03 1.67180-11 4.56950-01 -5.27770-03 3.92670-15 -3.87620-06
The same of the sa	3.56040-04-04-3.648±D-048.7827D-127.1985D-02
	9.7499D-09 -7.6750C-08 -1.6598D-09 -2.9252D-10 -6.5721C-05 1.7691D-05 -3.5292D-10 -5.7082C-04
	-1.55550-C6 2.73590-09 -9.62696-11 -1.2531D-09 -4.27946-08 -6.71430-09 6.80536-07 1.78370-08 -3.00360-09
	3
	MODE SHAPECORRESPONDING TO NATURAL FREQUENCY 1.44 96D 03 CYC./SEC.
	-0.46266-08 -3.1303D-09 1.46216-10 1.0385D-06 -2.2442D-09 6.17546-11 -1.8122D-09 -1.77866-09 1.26036-11 2.52016-13 7.15076-13
	-1.24130-08 -8.33860-07 -3.09510-06
	2.51460-09 -4
	-2.7524D-02 1.19555-07 -1.9394D-04 1.02635-05 -5.13686-03 -1.0407D-03 -4.5471D-01
	3.0515L-12 9.8095n-15 -3.3881C-12 -1.1588D-06 5.0697D-03 3.9327D-06 1.4091D-04 -8.4443D-01 -1.8961D-02 2.7989D-05
	MODE SHAPECORRESPONDING TO NATURAL FREQUENCY 1.4250D 03 CYC./SEC.
	i
	02 -5.6472C-12'-2.2546D-14 6.2746D-13 -6.4488C-01 -3.5321C-1
	-9.5585550-02 1.77345-11 8.45155-13 9.10610-02 -1.25645-11 9.75685-13 3.97735-01 -2.06685-12 8.45405-15 3.37215-01
	-1.5416D-15 -4.6342C-17 -1.5002D-06 5.99609-08 5.8715D-11 -2.2638D-05 -9.5474D-06 -
•	MODE SHAPECORRESPONDING TO NATURAL FREQUENCY 1.39350 03 CYC./SEC.
	44 40 10 10 10 10 10 10 10 10 10 10 10 10 10
	2.21200-03 3.75900-12 -6.52827-02 1.16100-02 -6.14750-13 3.01880-01 1.72840-03 -5.45510-12 -7.88135-01 4.84230-02 2.03550-13 -2.03550-13 -2.03550-1 7.86370-03 -1.47900-13 -1.47580-01 4.10920-03 3.77880-13 -1.09450-01 6.84460-04 4.16920-14

mir dere menten ander inter	5.6740D-05 -8.8249D-08 6.6536D-05 3.3370D-04 2.6065D-06 -5.5159C-07 6.
30	
72-0 50	1.23375-03 +9.71446-11 +2.00600-10 +4.66585-04 1.60595-10 6.6101D-12 4.6649D-05 +7.55
120R: ge A-	1.55720-10 -5.5750C-04 -3.77920D-1C 3.6414D-10 -1.4217C-04 3.C578D-10 1.3005C-1C 5.2325D-09 1.581
*N8 Pa	-6-22040-04 -3-2059E-05 1-1479D-06 -5-4794D-03 3-453ID-96 1.7544D-08 -1.1732D-02 -5.7115D-07 8.1655D-09 2.55379D-09 -1.1732D-02 -5.7115D-07 8.1655D-09 -1.2756D-09 -1.2766D-09
	-1.1651D-03 1.28620-05 -7.64690-06 4.7147D-02 -7.6503D-06 5.60050-02 2.6944D-01 1.5350D-03 -1.4291D-03 6.7623D-02
	MODE SHAPE COPRESPONDING TO NATURAL FREQUENCY 1.6436D 03 CYC. / SEC.
	1/22800-07 2.04150-09 -1.2026D-10 -1.4158D-08 1.72106-09 -5.02800-11 1.65550-09 1.55070-09 -1.28030-11 -2.1578D-13 -6.4246D-13
- :	-2-47540-05 2-57860-09 8
	-4.21218-05 1.2628E-05 1.16248-08 -9.08518-09 5.49188-07 -7.85938-0
	.69910-04 4.0569C-07 -A.
	1.61970-02 -1.56590-01 3.17230-03 -6.8952F-02 1.57210-02 -8.9687D-04 1.42240-02 -1.0931D-0
	6.03100-12 -6.62350-15 -3.36140-14 -2.93540-06 6.44970-05 4.99720-08 9.68710-04 -1.37940-02 -3.04310-04 -3.62550-05 4.44320-02 -5.07820-04 2.30930-07 -1.27420-03 3.29210-07 4.96490-03 -7.15750-03 -5.19870-02 -5.30560-02 -2.02600-03
	:
	5.37990ml3 2.4669D-02 -1.4822C-03 6.13660-13 1.9892D-02 -5.7246C-04 1.0731D-12 1.7507D-02 -1.4209D-04 5.0839D-13 - 5.81660ml9
	1.56048-13 8.95376-05 6.15370-05 -9.72280-14 -3.06946-03 -4.9056D-04 4.1304D-66 2.3762D-12 7.2103D-
.: *	-3.09540-03 -
	#2.29746-C8 =1.80950-08 =1.84950-09 =4.27090-08 =1.09440-09 1.19850-08 1.37390-06 =3.00470-08 =1.52320-09 =3.21980-09 1.27350-11 1.52130-09 =3.21980-09 1.27370-11 1.52130-09 =3.21980-09 1.27470-11 1.52130-09 =3.21980-09 1.27470-11 1.52130-09 =3.21980-09 1.27470-11 1.52130-09 =3.21980-09 1.27470-11 1.52130-09 =3.21980-09 1.27470-11 1.52130-09 =3.21980-09 1.27470-11 1.52130-09 =3.21980-09 1.27470-11 1.27470-
	-2.20315-14 -6.35065-08 1.54035-17 4.5354D-11 -4.80235-11 -2.99585-10 -1.05505-10 5.52745-09 1.19575-10 -3.7058D-12
	-4.35440-C5 MODF SHAPECORRESPONDING TO NATURAL FREQUENCY 1.58090 03 CYC./SEC.
	•93900-12 1.77756-05 -8.45386-07 -4.60286-13 1.400A5-05 -3.55316-07 5.19970-14 1.12120-05 -8.08696-08 -3.55536-1
	-2.58280-10 2.4700C-03 -7.5460-09
	490f-10 4.39440-02 6.62500-05 1.4729p-14 -3.4296D-0

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7.52/50-10 -'.525-6107 -1.5(ccc-68 7.82738-10 -5.2859-11 1.54160-69 1.54280-11 1.654280-01 -5.65769-10 1.14460-11 6.26160-02 2.078980-12 2.20656-13 -1.20439-01 -7.96290-12 -1.97590-12 -2.98120-01 4.33930-12 -1.90490-12 -7.26040-02	2 7.1041n-13 2.5110E-01 -1.3160D-12 2.38680-12 2.3820D-01 1.5127D-12 8.38020-13 -7.1656C-06 1.37320-1	7.25265-03 -3.57246-14 2.31535-14 -1.44735-02 -2.01426-13 -7.	6-2792D-13 -9-9868D-01 -6-0619D-13 -7-6538D-13 3-4692D-01 6-47510-13 2-4465D-14 -3-2935D-02 -1-6797D-13 2-6923D-14 3-49720-03 -7-4134D-14 8-4173D-15 -3-6064D-04 -1-1212D-13 2-4314D-15 4-2783D-05 -9-4845D-14 2-8471D-15 -4-3734D-09	-1.37100-14MORT SHAPECORRESPONDING TO NATURAL FREQUENCY 1.6977D 03 CYC./SEC.	4.01770-09	 	.72250-02	-5.5244D-13 8.2253E-05 8.1098D-05 9.222nD-13 -2.6641E-03 -9.5720D-04			.827cU-11 -1.7274D-15 -2.6618U-19 1.1976D-05 -8.6477D-10 -5.214ED-11 -6	-6.86100-07 8.89710-05 5.6205D-04 2.99770-06 -2.41090-08 -	-2-44410-08	1.2753D-12 -4.4576C-14 -1.5210D-01 -1.1122D-13 2.9342D-15 -1.0332D-01 2.9854C-14 1.0232D-13 1	2.39230-14 1.4256C-01 -3.42030-13 -8.99940-14 -7.00940-02 6.19180-13 -4.87560-14 1.01910-06	-7.42560-14 -3.11250-15 3.61810-13 -4.68640-02. 1 S.07130-14 4.04081-13 1	2.22870-13 6.56480-15 1.52060-05 1.78910-13 6.76800-15 -1.43190-06 2.32530-13 4	 **************************************	1.13965+(7 -1.01990-09 1.32735-07 -1.01650-05 1.32740-07 -1.12300-05 -8.45870-05 -3.41970-07 -4.07860-09 1.13915-05		1.29910-163.74440-918.22940-142.32280-145.89970-01-9.01500-142.93810-152.88750-0		3 -6.25930-14 -8.63810-1	3:20336-044:88240-144:89326-152.28036-05-05-5.0615P-14-7.47536-17-1:92566-06-14-2.26966-15-1:44566-10	1.52725-14

TILEN AMODE: SHAP FILL CORRESPONDING THO MATURIAL F REQUENCY TIME 12250 03 CYC./SEC.

elektrikalis dir. Bergenmann gembin gezeiche der villigen	-1-27540- 52-55460-03 1-93420- 43-66560- 52-45860- 6 -
30	1.0778p-14 -3.5576b-01 1.1914b-13 -1.1875p-14 -8.8638p-02 -3.1358b-13 -6.8972p-16 2.4597b-07 2.0290b-
72-0 ·52	1.21879-04 -1.6318E-12 -6.52220-15 -7.8941D-02 -3.4151E-14 2.3601D-1
20R e A	5-12280-10 -5-44690-12 4-1043C-09 -1.28690-07 4-16460-69 -1.37880-07 2.48490-07 -2.86340-09 -1.19810-10 -1.37200-66
	MODE SHAPECOPPESPONDING TO NATURAL FREQUENCY 2.3985D 03 CYC./SFC.
	-1.71260-14
	-5.7928U-10 -5.37820-14 -1.2795C-15 2.72230-11 2.04040-14 1.2783C-15 -1.5172D-12 -1.0822D-13 -1.0035D-15 -8.1989D-14
	-6.0820C+13. 1.86830-06 2.9991C+13 8.2028D-14 -2.78050-07 -2.1037D-14 -1.5267D+15 1.2028D-06 1.5190C-14 8.1875D-16
	-5.4545C-14 5.94200-16 -4.37520-09 3.96670-16 0.6779D-15 -5.41810-12 -4.5852C-06 8.2086D-1
	1.24425-03
	•24350-03 5.82990-
	1.33×70-05 -1.35×90-07 -4.6271E-05 -3.14890-03 -4.62740-05 -3.3809E-03 9.61940-01 -7.17660-05 -2.92650-06 -8.15410-01
	AMDDE SHAPE
	2.77910-14 -5.87500-03 -6.11250-04 1.30110-14 7.83030-03 -3.61610-04 2.38330-14 1.28400-02 -1.24510-04 1.10460-15 2.34750-06
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	-1.24730-13 2.36450-05 3.60950-05 2.21030-
	1.4665D-13 -6.5409D-02 -1.3532D-02 -1.
-	-7.00350-10 -1.25450-10 -1.65296-10 7.99400-09 1.28600-10 6.36890-11 -3.68930-07 7.22550-09 -5.81150-12 4.86240-10
	-i.10260-16 -2.50310-08 6.74120-19 -7.19390-12 3.77170-12 9.06140-11 -1.04020-11 -1.01050-10 -1.43590-12 9.74690-12 -1.44210-1442151-10-4.75540-12-2.82370-14-4.33610-12-2.194690-11
	-1.04610-04MODE SHAPFCORRESPONDING TO NATURAL FREQUENCY 2.1340D 03 CYC./SEC.
	01 -1.60110-02 1.45180-13 5.65930-01 -5.47610-02 -4
	-1.13464-03 -2.40950-13 -3.6695C-03 -7.39950-04 -3.80407-13 6.762CC-02 5.60520-04 -4.31920-14 -1.09360 00 -1.10770-02
	6.1155D-04 7.1965D-14 -1.0729D-03 -4.5290D-04 -1.7502D-14 -4.4629D-04 -4.7482D-04 G.
•	-1.58522-04 6.54708-05 4.8421P-14 1.75590-04 -6.91386-04 2.03848-13 1.52088-02 2.78568-04 1.
	-1-18556-11 -2-74680-13 -4-86120-16 -7-56230-08 1-54770-08 6-12750-13 4-64610-05 -2-674
	3 7.4031D-1

1.02830-14 -2.30390-20 -9.273-365000-12 2.95380-09 -8.75-2.222000-12 2.95380-06 7.633-4.10700-10 2.73930-14 -1.133-2.07610-14 -9.66360-16 -4.666-9.271-9.5690-09 -9.571-9.5690-09 -9.571-9.5900-09 -9.571-9.5900-09 -9.571-9.5900-09 -9.571-9.5900-19 3.01060-15 3.03-15-2.571-9.571	4.37546-14 2.19170-14 -3.65390-08 1.96146-14 1.00440-14 -4.37076-13-1.14219-13-3.56350-07-5.80840-14-2-6.6590-151.66246-15 2.69050-11 -1.61650-13 -7.328350-16 -1.42150-12 2.96386-26 -9.27440-06 8.10120-14 2.22550-13 2.93070-06 2.96386-09 -8.75350-08 2.96400-09 -9.33450-08 7.07080-06 2.72436-09 -8.75350-08 2.96400-09 -9.33450-08 7.07080-06 2.72436-06 -1.13820-13 2.9630-05 2.41926-08 7.07080-06 2.07036-14 -1.13820-13 2.9630-05 -2.41926-05 2.52530-09 -4.69626-16 -4.55910-01 2.30110-13 7.75280-15 2.65230-07 -4.69626-16 -2.71580-16 -5.42840-03 -5.55180-15 2.61200-16 4.9036-15 -2.71580-16 -5.42840-03 -5.55180-15 2.61200-16 2.01066-15 3.02040-06 3.80980-15 1.89246-15 -1.56230-07 -1.28210-13 1.06320-14 4.02430-13 -2.26020-17 -1.28210-13 -2.11820-08 1.86286-11 4.20120-13 -2.76970-02 -2.26020-07 -9.78770-08 1.86286-11 4.20120-13 -2.76970-07 -2.78000-07 -2.0000-07 -2.0016-12 -2.02200-12 -2.26070-07 -2.78000-07 -2.0000-07 -2.0016-12 -2.02200-12 -2.78000-07 -2.78000-07 -2.78000-07
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-8.08940-07 3.46910-21	
9.83400-15 -3.95465-14 1.47140-14 1.60760-15 1.24565-131.15760-13	
2.003EU-15 -1.00050-14 -5.65020-15 -2.13867-15 -5.92637-15 -6.83140-11 1.27890-11 2.83180-15 9.01660-08 -3.73020-08 1.0225U-14 -6.60500-07 2.09380-15 5.03800-15 5.57620-06 -7.89610-06 -4.42720-15 -1.07800-05 1.16410-05 -1.12170-14	
1.18550-05 -1.98340-05 -1.15696-14 -1.18070-05 2.89610-05 -5.75060-15 -1.06790-05 -3.90760-05 -1.36160-15 6.47190-12 1.02470-12 -9.91670-15 -8.71130-09 -2.18350-08 -1.04120-15 7.90360-07 9.09060-07 -1.52250-09 -4.67540-15 5.25800-05	
-7.68240-05MODE SHAPECORPESPONDING TO NATURAL FREQUENCY 2.7616D 03 CYC./SEC.	
-1.557kD-14 1.0633D+15 2.5570D-19 2.3597D+08 -3.2791D-14 -4.5318D-14 -6.4086D-09 1.9643D-12 -2.7359D-13 1.2558D-08 -22.3051D-11 1.55965-12 -6.0257C-10 1.0325D-08 -6.0257C-10 1.08645D-10 1.0865D-10 1.0865D-10 1.0865D-10 1.0	T Commence and the commence of
1.8a195-11 -4.04435-07 -6.61805-11 8.39435-10 5.61035-06 -2.29505-10 -2.62730-11 -1.24400-10 -	
-5.63870-15 2.0955C-16 3.8986N-01 1.848RN-15 -	
1.7841D-04 -3.4693C-15 1.2187D-17 -1.2569D-03 -4.8786D-15 -9.35529-18 9.3898D-18 -8.3287C-02 -3	
5.98980-14 9.54500-16 1.	
MODE SH	
-3.9394D-15 -6.8620C-15 -1.3380D-08 2.5735D-01 3.3108C-10 -2.0326D-08	
-2.54716-03 8.23150-05 8.21450-07 7.04100-05 -1.97500-06 -1.91896-07 -1.75350-06 1.29950-07: 2.23350-06 2.76780-66 -1.7538100-08 1.81880-10 9.23370-10 -7.30720-11 4.14176-11 2.91116-11	•
1.04c1D-12 -3.1076D-13 -6.2847C-14 -2.2670D-12 8.6C41D-14 4.2697C-14 2.7482D-12 -2.8105C-14 -2.4772C-14 -2.4387D-12 -4.0173D-14 1.28660C-14 1.4230C-12 -5.2349D-14 -2.0235D-15 -1.5710C-13 4.7921D-14 -4.5995D-15 6.3658D-17 9.7564D-15	•
3.05500-15 -3.22780-15 1.49030-15 1.33940-14 2.55150-13	¹N P
-1.21797-13 1.9046D-15 -4.1147D-15 -3.8204D-14 3.53975-15 -2.8525D-14 8.2622D-14 3.3912D-15 2.	8120R age A
SHAPE.	72-0 54
61,-7376P-136,3303D-143,3301D-143,2961D-156-8,0714P-142,2961D-143,0067D-13-1,2779D-14	30
7.3820p-15 5.5540D-13 1.0405p-14 7.8650p-15 1.2442C-08 -2.3005p-09 5.9442p-14 -1.8714b-05 7.	

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	2.62410-15
	3.9063D-15 3.74810-14 -2.9862D-16 5.0448D-15 -6.1726D-15 2.5131D-16 -5.85
20R e A-	-3.64590-16 1.05600-09 5.53820-10 -1.15990-15 -3.72350-11 -1.00660-12 -3.88240-17 3.82470-15 -5.52780-14
	-5.67250-10 -2.66260-17 1.90860-07 5.68330-09 -1.87720-16 -1.20760-05 3.19780-10 5.95940-17
_	6.35000-12 -2.75100-12 2.51780-16 -6.23750-11
	-4.26476-14 -2.13446-15 -1.86676-12 -4.26470-14 -4.44068-16 -1.23236-05 5.19950-14 -4.32356-17 1.62446-08 -3.36246-10
	7.9958D-09 2.5826D-10 6.8190D-16-
	3.50350-14 4.8RA60-15 -1.17920-13 4.29920-14 -1.19110-13 -4.9960-13 3.76180-14 4.19960-13 4.37920-14 2.44950-14
	4.15206-18 -5.39110-17 4.65655-21 1.79405-14 -4.94215-15 -9.74760-18 -1.43790-14 1.40140-13 4.61835-15 -1.13615-14
	MODE SHAPE CORRESPONDING TO NATURAL FREQUENCY 5.0324D 03 CYC./SEC.
·	1.5516P-15 -2.3032D-16 5.6983D-14 -2.8764D-16 1.7095D-18 7
	-2.15466-15 6.08260-15 2.55486-15 2.54500-16 6.61320-15 2.28750-15 7.64690-17 -2.44850-13 +6.05050-15 6.01370-15
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	-8.37420-16 -1.42260-15 8.99460-17 1.75410+11 -1.28500-06 -1.04280-09 1.61810-09 2.05330-03 7.09410-05 -1.14350-08
	MODE SHAPECOPRESPONDING TO NATURAL FREQUENCY 4.40120 03 CYC./SEC.
,	
•	-1.93830-1
	-2.02710-15 -3.4704D-03 -3.1091D-05 2.8773D-14 1.9166E-01 3.
	3.7579D-14 1.8274D-12 4.15766-11 -3.46875-15 1.09119-09 -3.02549-09 -3.02310-11 -2.27585-14 1.
	9.0510D-08 +5.5588D-08 4.4288C-15 -2.1194D-07 2.2847D-07 2.8148D-16 -1.
	5.69590-11 -1.66050-11 -2.31010-15 -9.80570-10
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